

If you would like previous copies of Technical News, please complete the following form and **fax to NHP on (03) 9429 1075** to the attention of the **Marketing Department**.

Name: Title: Company:

Please post to: address

Telephone: () Fax: ()

Please email to:

Other issues currently available.

Please tick those you would like to receive.

- | | | |
|--|---|---|
| <ul style="list-style-type: none"> <input type="checkbox"/> 1. First edition (Latched and delayed contactors) <input type="checkbox"/> 2. Non-standard contactor applications (Parallel and series connections of contacts varying frequencies) <input type="checkbox"/> 3. Contactor failure (Reasons for the failure) <input type="checkbox"/> 4. Soft start for generator loads (Advantages of electronic soft starters) <input type="checkbox"/> 5. Set the protection (MCCB breakers and application) <input type="checkbox"/> 6. Contactor operating speed (Difference between AC and DC systems) <input type="checkbox"/> 7. Quick guide to fault levels (Calculating the approximate fault levels) <input type="checkbox"/> 8. IP ratings what do they mean? (IP Ratings, use and meaning) <input type="checkbox"/> 9. Utilisation categories (Electrical life of switches) <input type="checkbox"/> 10. AC variable frequency drives and breaking (Regenerative energy) <input type="checkbox"/> 11. Don't forget the motor protection (Motor protection devices and application) <input type="checkbox"/> 12. Electrical life of contactors (How and why contactors are tested) <input type="checkbox"/> 13. Liquid resistance starter developments (For large slipping motors) <input type="checkbox"/> 14. Taking the 'hiss' out of DC switching (DC switching principles) | <ul style="list-style-type: none"> <input type="checkbox"/> 15. Start in the correct gear (Application of different motor starters) <input type="checkbox"/> 16. Application guide to lamp selection (Industrial pushbutton controls) <input type="checkbox"/> 17. Electrical surges can be expensive (Electrical surges) <input type="checkbox"/> 18. Putting the PLC in control (advantages of the PLC) <input type="checkbox"/> 19. The thinking contactor (The development of the contactor) <input type="checkbox"/> 20. Some don't like it hot (Temperature rise in electrical switchgear) <input type="checkbox"/> 21. Pollution of the airwaves (Unwanted signals and their effects on motor protection devices) <input type="checkbox"/> 22. What's different about safety? (Safety devices and their application) <input type="checkbox"/> 23. Talk about torque (Motors and torque) <input type="checkbox"/> 24. Power factor what is it? (Power factor and correction equipment) <input type="checkbox"/> 25. Terminations, good or bad? (Terminals) <input type="checkbox"/> 26. RCDs are saving lives (Earth leakage protection; RCDs) <input type="checkbox"/> 27. The quality switchboard (Switchgear and protection devices for Switchboards) <input type="checkbox"/> 28. How does electrical equipment rate (Understanding ratings of electrical equipment) <input type="checkbox"/> 29. EMC - what's all the noise about (Understanding EMC) <input type="checkbox"/> 30. Controlling high short circuit currents with current limiting circuit breakers (Short circuit co-ordination KT 7) | <ul style="list-style-type: none"> <input type="checkbox"/> 31. Another step in electrical safety (Changes to electrical safety) <input type="checkbox"/> 32. Keep your cables cool (New requirements on cable protection) <input type="checkbox"/> 33. A leak to earth can be electric (RCDs) <input type="checkbox"/> 34. Keep Cool (Derating) <input type="checkbox"/> 35. Improving star-delta protection. (Overload and short circuit protection) <input type="checkbox"/> 36. Does your CT measure up? (Selecting the correct current transformer) <input type="checkbox"/> 37. Is your copper flexible? (Flexible busbars) <input type="checkbox"/> 38. Where did the 10 volts go? (world uniform voltages) <input type="checkbox"/> 39. Motor protection and wiring rules (overload protection) <input type="checkbox"/> 40. Confused about which RCD you should be choosing? <input type="checkbox"/> 41. Circuit breakers working together <input type="checkbox"/> 42. Keeping in contact. <input type="checkbox"/> 43. Is your switchboard in good form? <input type="checkbox"/> 44. Automation in a technological world <input type="checkbox"/> 45. Thermal simulation of switchgear <input type="checkbox"/> 46. Cable Considerations <input type="checkbox"/> 47. Output chokes for use with variable speed drives <input type="checkbox"/> 48. VSD Installation Techniques <input type="checkbox"/> 49. The modern Scada System <input type="checkbox"/> 50. 50th Edition Special <input type="checkbox"/> 51. Electrical design considerations for commercial buildings |
|--|---|---|

TNL is available as a download from NHP's Online Resource Centre (OCR), visit nhp-online.com.au The OCR provides members with up-to-the-minute technical information and powerful product tools, all at the click of a mouse button. Register for membership today!

Editorial content: - Please address all enquiries to: The Editor - 'NHP Technical News' PO Box 199, Richmond, Victoria, 3121.



nhp.com.au

nhp-nz.com

NHP ELECTRICAL ENGINEERING PRODUCTS PTY LTD

A.B.N. 84 004 304 812

MELBOURNE +61 3 9429 2999	LAVERTON +61 3 9368 2901	SYDNEY +61 2 9748 3444	CAMPBELLTOWN +61 2 9748 3444	NEWCASTLE +61 2 4960 2220	CANBERRA +61 2 6280 9888	ALBURY +61 2 6056 4318	BRISBANE +61 7 3909 4999	TOWNSVILLE +61 7 4779 0700
ROCKHAMPTON +61 7 4927 2277	TOOWOOMBA +61 7 4634 4799	CAIRNS +61 7 4035 6888	ADELAIDE +61 8 8297 9055	PERTH +61 8 9277 1777	DARWIN +61 8 8947 2666	HOBART +61 3 6228 9575	AUCKLAND +64 9 276 1967	CHRISTCHURCH +64 3 377 4407



Environmentally Friendly
Printed on recycled paper



[ISSUE 52] JANUARY 08
**TECHNICAL
 NEWS**

INDUSTRIAL SWITCHGEAR & AUTOMATION SPECIALISTS



Terminal temperatures

How hot are they?

Excessive temperatures are often the cause of failures in electrical equipment. High temperatures can cause the degradation of insulating materials, the failure of joints and a reduction of strength. Unfortunately the standards for electrical equipment can lead the unwary in to applying switchgear in a manner that will lead to high temperatures and possible failure. Fortunately most electrical equipment runs at currents less than the design maximum and service problems do not arise. However, in applications required to withstand high loadings for long periods there can be a high risk of failure.

CURRENT RATING

All electrical switchgear has a current rating assigned to it. It is marked on the device and looks simple enough. It should however have a warning about this rating along the lines of, 'the current rating of this device is only nominal and was determined under test conditions that may not be matched in service. It is possible that when installed the installation conditions will be such that if run at the nominal current rating excessive temperatures will arise, a derating should be applied'.



Cables or bars? What's the difference?

FEATURING

- Current rating
- Comparison table
- Conductor ratings

Written by Bill Mairs

National Manager
 Technical Department

PLEASE CIRCULATE TO:

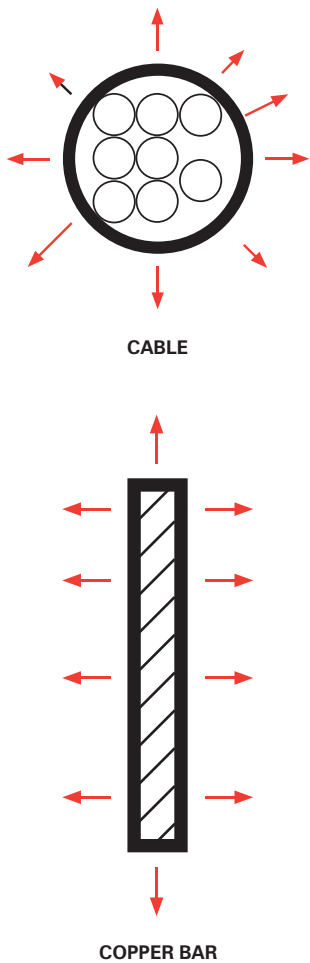


Fig 1
Bars provide larger surface area for cooling

For the purchaser a major point of comparison between devices from different suppliers is the price per amp. The standards set test conditions for current rating and this helps ensure these comparisons are valid. The problem is that the standard test conditions allow the best or highest nominal rating to be assigned.

Considering circuit breakers rated to AS60947.2 there are several ratings related to current.

1. Conventional free-air thermal current (Ith)
2. Conventional enclosed thermal current (Ithe)
3. Rated current (In)

The rated current (In) is required to be marked on the circuit breaker and is defined as being equal to the conventional free-air thermal current (Ith). The implication of this is that should the circuit breaker be mounted in an enclosure it will run hotter and may exceed permissible temperatures. The next issue in the test conditions specified for Ith the test connections are specified and these have larger cross sections than what might be selected for a conductor for the particular current (refer table 1 below).

While conventional testing does allow circuit breakers from different manufacturers to be compared it does complicate the application of the circuit breakers. Failure to understand the issues can lead to excessive temperatures and reduced life.

HOW TO APPLY

The correct selection and installation of a circuit breaker in a switchboard to AS3439 Switchgear Assemblies is the responsibility of the switchboard manufacturer. This responsibility is defined in the standard. A warning that installed ratings may be different to the marked current In is also provided.

For an assessment to be made on the likely performance of switchboard equipment reference can be made to AS4388 (a method of temperature rise assessment). This standard outlines a method for determining the likely internal temperature rise in a switchboard. From this calculation adjustments can be made to equipment selection by applying deratings or selecting higher rated devices to achieve the required ratings. A table within the standard also highlights the need for conductors connecting directly to switchgear to be of generous proportions (refer table 1 below).

CONDUCTOR RATINGS

For a simple length of cable the current rating is determined by the permissible insulation temperature. This also applies to insulated flexible busbar. The typical maximum temperature being 105 ° C. For bare busbars the limit is again typically 105 ° C as this is considered the maximum temperature copper can reach without annealing taking place. Annealing can reduce the mechanical strength of the copper and reduce its ability to withstand forces produced by short circuits.

Table 1 Conductor sizes

Current amps	Device testing for Ith Standard test conductors		Typical cable selection to AS3008.1.1		Typical bar selection		Required bar size from AS 4388 Table B.3. 7/9	
	Size mm ² / mm x mm	x section mm ²	Table 6 Column 6	x section mm ²	105 deg max 45 deg ambient	x section mm ²	Device to busbar	x section mm ²
Cable								
125	50	50	50	50				
250	120	120	120	120				
400	240	240	240	240				
630	2 x 185	370	2 x 185	370				
800	2 x 240	480	2 x 240	480				
Bars								
125							1 - 20 x 3	60
250					1 - 12 x 5	60	2 - 20 x 5	200
400					1 - 20 x 5	100	1 - 30 x 10	300
630	2 - 40 x 5	400			1 - 40 x 5	200	1 - 50 x 10	500
800	2 - 50 x 5	500			1 - 50 x 5	250	2 - 30 x 10	600
1000	2 - 60 x 5	600			1 - 80 x 5	400	2 - 40 x 10	800
1250	2 - 80 x 5	800			1 - 80 x 5	400	2 - 50 x 10	1000
1600	2 - 100 x 5	1000			2 - 60 x 5	600	2 - 80 x 10	1600

Notes: Table prepared for comparison only. Refer to Standards or actual test data for conductor selection.
AS3008.1.1 Electrical installations - Selection of cables.

AS4388 -1996 A method of temperature-rise assessment by extrapolation for partially type-tested assemblies (PTTA) of low-voltage switchgear and controlgear.

The passage of current in a conductor causes internal heating and the temperature rises until the rate of heat dissipated by radiation and convection matches the heat input. The ability to dissipate heat depends on the cooling surface area. For a round conductor the cooling surface is at its minimum for a given cross section of copper. If a copper rod with a cross sectional area of 100 mm² is considered the cooling area per cm length is 113 mm² but a 100 mm² copper bar of dimensions 5 x 20 mm has a cooling area of 500 mm² per cm length. The result is that while the rod and the bar have the same amount of copper the bar can run at a higher current because of the better cooling provided by the larger surface area (refer fig 1 far left).

THE HEAT SINK

During thermal testing, cables are specified for use with breakers rated 400 A and below. The cable core temperature in these tests is lower than the specified maximum temperature for the terminals. Heat will flow from the circuit breaker into the cable and therefore help control the temperature rise of the terminals. When a bar is used instead of cable and it has better cooling properties, its cross sectional area can be smaller than a cable. While the temperature rise of the bar and the cable may be the same, at a distance from the breaker, the ability of the bar to heat sink the terminals is less than the cable due to the smaller cross section. As an example, the test for a 400 A circuit breaker requires 240 mm² cables. This cable will have a temperature rise of about 35 ° C. If a bar was selected for a 35 ° C rise at 400 A, a 30 mm x 5 mm bar could be selected. This bar has a cross section of only 150 mm² and will not provide the required heat sinking (refer fig 2 right).

BUSBAR TO DEVICE CONNECTIONS

The need to provide heat sinking to achieve circuit breaker ratings is recognised in AS4388. Bar sizes are listed for the link between the circuit breaker and the main busbar system. The sizes are comparatively larger than might be expected but are generally in line with the sizing of standard test conductors specified in the circuit breaker standard.

Cables connecting to circuit breakers do not normally present a problem. If cables are selected from Table 6, Column 6 of AS/NZS3008.1.1 then the sizing should be adequate. Cables with high temperature insulation should not be run at the claimed higher current ratings assigned to these cables but should be applied in accordance to Table 6.

INSTALLED RATINGS

In addition to consideration of the conductor sizes care must be taken with the enclosure. Depending on the design of the circuit breaker it may or may not have been tested for rating when mounted in an enclosure. Even if tested in an enclosure its arrangement in service may cause extra heating and a derating may need to be applied. A 20 % derating when installed in a switchboard would be typical. As the current goes up the greater the care needed in assessing the installed rating.

CONDUCTOR COMPARISONS

In Table 1 (refer page left) a range of conductor selections is shown. The first column lists the standard test conductors from the AS/NZS3947 Switchgear standard series. From this table it can be seen that for cables there is not a significant problem. Sizing for the rating test is much the same as if cables are selected from Table 6 of AS/NZS 3008.1.1. When it comes to using bars there is a significant difference between the cross section of bar selected for normal use and a bar used for the device standard test. The in-service recommended sizes in AS4388 must be used to prevent overheating by providing a heat sink.

OTHER DEVICES

While circuit breakers have been discussed above most other switchgear devices face the same issues.

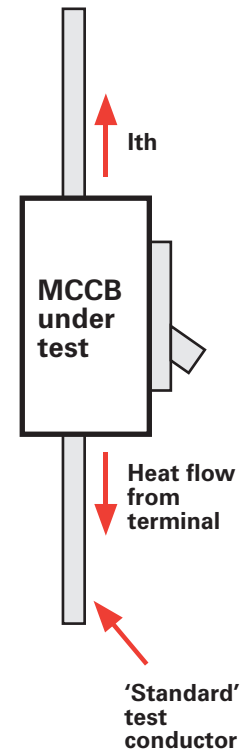


Fig 2
Test conductors provide a heat sink to terminals